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# MIMO-PID Controller For Deregulated environment

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Abstract: This assessment represents a Multi-Input-Multi-Output-Proportional-Integral-Derivative (MIMO-PID) controller for load frequency balance issues. The objective of load frequency control is to minimize the transient deviations in area frequency and tie-line power. To improve the robustness of the system the transfer function  $H_{\infty}$  norm is used. So the proposed technique is known as PIDH<sub> $\infty$ </sub> controller. The LFC problem is articulated as a H<sub> $\infty$ </sub> SOF (State Output Feedback) control approach to attain the decentralized robust MIMO-PIDH<sub> $\infty$ </sub> controller. H<sub> $\infty$ </sub> controller is used here for accomplishing stabilization with definite performance. The optimization difficult is formulated and iterative LMI algorithm is used to tune the control parameters of the MIMO-PIDH<sub> $\infty$ </sub> controller. The simulation results show the proposed strategy is very effective and guaranteed good robust performance against the parametric uncertainties and load changes.

Keywords: H<sup>∞</sup> control; LMI; Area Control Error; Load Frequency Control; MIMO-PID control.

## I. INTRODUCTION

In electrical power system due to deregulation there are PID Controller defined as: unrivalled changes in system and theyraise to changes in the competitive market. The role of control in power system (either man-made operation or instinctive) is to shield operation by returning when subjected to disturbances. In other words control in power system means continuing of system within soothed limits of performance to disturbances, such as short circuits and generation loss or load loss.Lot of study is carried out and on work about this LFC in restructured power system [1]-[8]. With vibrant and bilateral contracts researchers have modified AGC conventional one [1]-[3]. New market schemes and their operational tools are proposed in [2]. Modified AGC is presented in [4]. LMI approach with decentralized strategy proposed in [7]. Neuro-fuzzy adaptive control is proposed in [8]. In this research threearea power system is specified as dynamic model. The distribution companies (DISCOs) can contact generation companies (GENCOs) for their power needs with different area contracts under independent service operator (ISO). For contract execution a matrix DISCO participation matrix (DPM) is used for conception [4]. The control PID problem is reduced through static output feedback problem is formulated as H<sup>∞</sup> static output feedback (SOF) (SOF) control system as control approach to get novel decentralized MIMO-PID controller based on LMI algorithm. The robustness of proposed controller shown through simulation results.

#### **II. PROPOSED CONTROL STRATEGY**

In this section momentary view of decentralized MIMO-PIDH∞ control through LMI is followed

System model defined as:

$$x = Ax + B_1w + B_2u$$

 $z_{\infty} = C_1 x + D_{12} u$ (1) $y = C_2 x$ 

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$$u = K_1 y + K_2 \int_0^t y dt + K_3 \frac{dy}{dt}$$
 (2)

Here K1,K2,K3 matrices are to be designed (PID Gains) Output feedback H∞-control problem is to find controller of

$$u = Ky \tag{3}$$

From above closed loop transfer function of infinite-form from  $Z\infty$  to w

$$(||T_{z_{\infty}^{w}}||) < \gamma \tag{4}$$

Consider 
$$z_1 = x z_2 = \int_0^\infty y dt$$
 and  $z = \begin{bmatrix} z_1 \\ z_2 \end{bmatrix}$ 

The variable as viewed state vector of new system

$$z_1 = x = Az_1 + B_1w + B_2u$$
  

$$z_2 = C_2z_1$$
 (5)  

$$z_1 = x = C_1x + D_{12}u$$
 (6)  
PID problem is reduced threa

$$z = \overline{A}z + \overline{B_1}w + \overline{B_2}u$$

$$\overline{z}_{\infty} = \overline{C}_1 z + \overline{D_{12}}u$$

$$\overline{y} = \overline{C_2}z + \overline{D_{21}}w$$

$$u = \overline{K}\overline{y}$$
Where
$$\overline{A} = \begin{bmatrix} A & 0\\ C_2 & 0 \end{bmatrix}, \ \overline{B_1} = \begin{bmatrix} B_1\\ 0 \end{bmatrix}, \ \overline{B_2} = \begin{bmatrix} B_2\\ 0 \end{bmatrix},$$

$$\overline{C_1} = \begin{bmatrix} C_1 & 0 \end{bmatrix}, \overline{C_2} = \begin{bmatrix} \overline{C_{21}} & \overline{C_{22}} & \overline{C_{23}} \end{bmatrix},$$

$$\overline{D_{12}} = D_{12}, \ \overline{D_{21}} = \begin{bmatrix} 0 & 0 & C_2 B_1 \end{bmatrix}, \quad (7)$$
And
$$\overline{K} = \begin{bmatrix} \overline{K_1} & \overline{K_2} & \overline{K_3} \end{bmatrix}$$

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(8)



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Once  $\overline{K}$  is found original PID gains can be obtained

 $K_3 = \overline{K_3} (I + C_2 B_2 \overline{K_3})^{-1},$  $K_2 = (I - K_3 C_2 B_2) \overline{K_2}$ (9) $K_1 = (I - K_3 C_2 B_2) \overline{K_1}$ 

LMI algorithm for PIDH, optimizing system in equation Controlled output vector considered as follows (4) follows

Step 1: From state space model in (1)

Compute  $\overline{A}$ ,  $\overline{B_1}$ ,  $\overline{B_2}$ ,  $\overline{C_1}$  and  $\overline{C_2}$  by using (7) and select performance index ( $\gamma$ )

Select Q>0 and solve for riccati equation Step 2:

$$\overline{A}^T P + P\overline{A} - P\overline{B_2}\overline{B_2}^T P + Q = 0, P > 0$$
  
Set  $i = 1$  and  $X_i = P$ 

Step 3: solve optimization problem for  $P_i$ , K and  $a_i$ Optimization 1: minimize ai subject to LMI constraints

Σ	$P_i \overline{B_1}$	$(\overline{C_1} + \overline{D_{12}} \overline{K} \overline{C_2})^T$	$(\overline{B_2}^T P_i + \overline{K}\overline{C_2})^T$	
$\overline{B_1}^T P_i$	-γ	0	0	< 0
$\overline{C_1} + \overline{D_{12}}\overline{K}\overline{C_2}$	0	$-\gamma$	0	
$\left[\overline{B_2}^T P_i + \overline{K}\overline{C_2}\right]$	0	0	- I	
			(10)	

Where  $\sum_{i=\overline{A}^{T}P_{i}+P_{i}\overline{A}-X_{i}\overline{B_{2}}\overline{B_{2}}^{T}P_{i}-P_{i}\overline{B_{2}}\overline{B_{2}}^{T}X_{i}+X_{i}\overline{B_{2}}\overline{B_{2}}^{T}X_{i}-aP_{i}$ 

 $a_i^*$  Denotes minimized value of  $a_i$ 

Step 4: If  $a_i \leq 0$  the matrix pair  $(P_i, \overline{K})$  solves the problem. Stop. Otherwise go to step 5

Step 5: solve optimization problem for  $P_i$  and  $\overline{K}$ 

Optimization 2: minimize P<sub>i</sub> subject to LMI constraint in (10) with  $a_i = a_i^*$ .

Optimal  $P_i$  denoted by  $P_i^*$ 

Step 6: If  $||X\overline{B_1} - P_i^*\overline{B_1}|| \le go$  to step 7 otherwise set i = i + 1,  $X_i = P_i^*$  and go to step.

Here  $\in$  denotes tolerance (prescribed)

Step 7: If obtained K satisfies gain constant, it is desirable otherwise change weight  $n_i, Q$  and  $\gamma$  go to step 1.

#### **III.DESIGN MODEL OF CONTROLLER**

Projected model for three area power system with interconnections in deregulated background as [4] and [8] is shown in Fig 1.

State space model as follows:

 $x = \begin{bmatrix} \Delta X_{E1} & \Delta P_{t1} & \Delta f_1 & \Delta X_{E2} & \Delta P_{t2} & \Delta P_{tie12} & \Delta X_{E3} & \Delta P_{t3} & \Delta f_2 \end{bmatrix}$  $w = \begin{bmatrix} \Delta P_{L1} & \Delta P_{L2} & \Delta P_{L3} & \Delta P_{L4} & \Delta P_{L5} & \Delta P_{L6} \end{bmatrix}^T$  $u = \begin{bmatrix} u_1 & u_2 & u_3 \end{bmatrix}^T$ 

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$$z_{\infty}$$
 is a controlled output vector

$$y = [ACE_1 \quad ACE_2 \quad ACE_3 \quad \Delta f_1 \quad \Delta f_2$$
$$\Delta f_3 \quad \Delta P_{tie12} \quad \Delta P_{tie23} \quad \Delta P_{tie31}]^T$$
y is a measured output vector

$$z_{\infty} = \begin{bmatrix} n_1 \Delta f_1 & n_2 \Delta f_2 & n_3 \Delta f_3 & n_4 \Delta P_{iie12} & n_5 \Delta P_{iie23} \\ n_e \Delta P_{iie21} & n_7 u_1 & n_9 u_2 & n_9 u_2 \end{bmatrix}^T (12)$$

Here  $n_1$  to  $n_9$  are constants and weight coefficients are chosen by designer.

Consider three area power system parameters in Fig 1. as  $K_g=1.0$ ,  $T_g=0.08s$ ,  $K_t=1.0$ ,  $T_t=0.3s$ ,  $R_i=2.4(Hz/pu)$ ,  $B_i=0.425(pu/Hz)$   $K_P=120(pu/Hz)$ , Tp=20s,  $T_{12}=0.0868s$ , T23=0.0868s, T31=0.0868s





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Figure 1. Three area power system with cpfs.

### **IV.RESULTS**

Free contracts transactions based scenario:

In this section all DISCOs are contracted with GENCOs as per DPM (Dynamic Participation Factor).

DPM =	0.5	0.25	0	0.3	0.8	0 ]
	0.2	0.25	0	0	0.1	0.1
	0	0.25	1	0.7	0.1	0.1
	0.3	0.25	0	0	0	0.8

All GENCOs in each area participate as follows

apf1=0.50 apf2=1-apf1=0.50

apf3=0.50 apf4=1-apf3=0.50

apf5=0.50 apf6=1-apf5=0.50

Load variations considered as

 $\begin{array}{cccc} \Delta P_{L1}{=}0.75pu & \Delta P_{L2}{=}0.75pu & \Delta P_{L3}{=}0.75pu \\ \Delta P_{L4}{=}0.75pu & \Delta P_{L5}{=}0.75pu & \Delta P_{L6}{=}0.75pu \\ \Delta P_{M1}{=}0.5{*}0.75{+}0.25{*}0.75{+}0{*}(0.75){+}0.3{*}(0.75){+}0{*}(0.75) \\ {+}0{*}(0.75){=}0.7875pu \end{array}$ 

Correspondingly

 $\Delta P_{M2} = 0.3375 pu \quad \Delta P_{M3} = 0.4275 pu \quad \Delta P_{M4} = 0.4125 pu \\ \Delta P_{M5} = 0.5475 pu \quad \Delta P_{M6} = 0.1500 pu$ 

Power generated from GENCOs in area-I, II and III shown in Fig 3. With desired values of  $\Delta P_{Mi}$ . Test results show robustness of the system.



Figure2. Frequency deviations in corresponding areas



Figure3. Generated Power

## **V.** CONCLUSION

In three area power system with reheat type thermal power stations this researchoffers MIMO-PID decentralized controller in restructured power system. To diminish effects of uncontrolled changes in system in area's inside loads and in interconnected loads control actions are calculated through LMI. For guaranteed performance and robustness this controller is effective and efficient against variations in loads and parametric uncertainties.

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